MINIMIZATION OF MISMATCH IN METAL HOLDING IN REVERBATORY FURNACES

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A solution of the problem of minimization of the deviation of an actual thermal process from the desired one in metal holding in a reverbatory furnace is suggested.

We consider the problem of heat treatment of a thermally thin body in a reverbatory furnace. The dynamics of temperature variation of the metal ingot and heating medium is described by the equations [1]:

$$\frac{dT_{\rm h}}{dt} = A_1 \nu - A_2 T_{\rm h} - A_3 \left(T_{\rm h} - T \right), \tag{1}$$

$$\frac{dT}{dt} = \mu \left(T_{\rm h} - T \right) \tag{2}$$

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with the initial conditions

$$T_{\rm h}(0) = T_{\rm h0}, \ T(0) = T_0.$$
 (3)

Let for the given thermal process the desired operating conditions of the heating device be given at v = . const.

We determine $T_h(t)$ and T(t)

$$T_{h}(t) = T_{h.inhom}(t) + T_{h.hom}(t), T(t) = T_{inhom}(t) + T_{hom}(t)$$

whence it follows that

$$T_{\text{h.inhom}}(t) = T_{\text{inhom}}(t) = \frac{A_1}{A_2} v, \quad T_{\text{hom}}(t) = C_1 \exp(k_1 t) + C_2 \exp(k_2 t),$$

$$T_{\text{h.hom}}(t) = C_1 \exp(k_1 t) + C_2 \exp(k_2 t) + \frac{1}{\mu} (C_1 k_1 \exp(k_1 t) + C_2 k_2 \exp(k_2 t)),$$

$$C_1 = \frac{(T_{\text{h0}} - T_0)\mu - T_0 k_2}{k_1 - k_2}, \quad C_2 = \frac{T_0 k_1 - (T_{\text{h0}} - T_0)\mu}{k_1 - k_2},$$

$$k_1 = \frac{1}{2} \left(-(A_2 + A_3 + \mu) + \sqrt{(A_2 + A_3 + \mu)^2 - 4A_2\mu} \right),$$

$$k_2 = \frac{1}{2} \left(-(A_2 + A_3 + \mu) - \sqrt{(A_2 + A_3 + \mu)^2 - 4A_2\mu} \right).$$

But a real thermal process with temperatures T_h^* and T^* differs, as a rule, from the desired one

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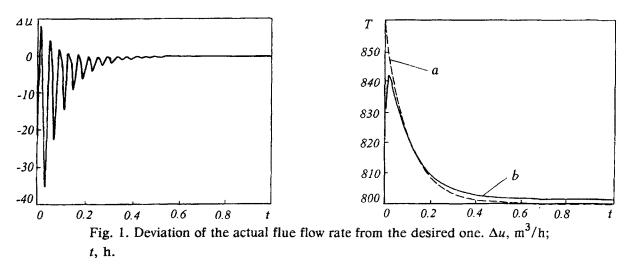


Fig. 2. Plots of time variation of temperatures of metal ingot (a) and heating medium (b). T, ^{o}C .

$$\frac{dT_{\rm h}^*}{dt} = A_1 v^* - A_2 T_{\rm h}^* - A_3 \left(T_{\rm h}^* - T^*\right), \ \frac{dT^*}{dt} = \mu \left(T_{\rm h}^* - T^*\right)$$

with the initial conditions not coinciding with (3):

$$T_{\rm h}^*(0) = T_{\rm h0}^*, \ T^*(0) = T_0^*.$$

Therefore, we face the problem of minimization of the mismatch obtained for the gas ΔT_h , and metal ΔT temperatures and for the fuel flow rate Δv :

$$\frac{d\Delta T_{\rm h}}{dt} = A_1 \Delta \nu - A_2 \Delta T_{\rm h} - A_3 \left(\Delta T_{\rm h} - \Delta T\right), \quad \frac{d\Delta T}{dt} = \mu \left(\Delta T_{\rm h} - \Delta T\right),$$
$$\Delta T_{\rm h} \left(0\right) = \Delta T_{\rm h0}, \quad \Delta T \left(0\right) = \Delta T_0, \quad \int_0^{t_{\rm f}} \left(\alpha \Delta T_{\rm h} \left(t\right)^2 + \beta \Delta T \left(t\right)^2 + \gamma \Delta \nu \left(t\right)^2\right) dt \Rightarrow \min$$

where $\Delta T_{h} = T_{h} - T^{*}$; $\Delta T = T - T^{*}$, $\Delta v = v - v^{*}$; $\Delta T_{h0} = T_{h0} - T^{*}_{h0}$, $\Delta T_{0} = T_{0} - T^{*}_{0}$. Having replaced the variables and denoting

$$\begin{aligned} x &= \begin{pmatrix} \Delta T_{\rm h} \\ \Delta T \end{pmatrix}, \quad u &= \Delta \nu, \quad A = \begin{pmatrix} A_2 + A_3 & -A_3 \\ -\mu & \mu \end{pmatrix}, \quad B = \begin{pmatrix} -A_1 \\ 0 \end{pmatrix}, \\ x_{\rm f} &= \begin{pmatrix} \Delta T_{\rm h0} \\ \Delta T_0 \end{pmatrix}, \quad P = \begin{pmatrix} \alpha & 0 \\ 0 & \beta \end{pmatrix}, \quad Q = \gamma, \end{aligned}$$

we pass to a problem of the form

$$\frac{dx}{dt} = Ax + Bu , \qquad (4)$$

$$x(t_{\rm f}) = x_{\rm f} , \qquad (5)$$

$$I(u) = \int_{0}^{t_{f}} (x^{T} P x + u^{T} Q u) dt \rightarrow \min_{u \in \mathbb{R}} .$$
(6)

Thus, in holding of a metal ingot in a furnace with a fixed temperature it is necessary to solve the problem of constructing a regulator of heating to the holding temperature if the temperatures of the ingot and of the heating medium deviate from the prescribed ones.

A method of solving the problem of analytical design of optimum regulators (4)-(6) is considered in [2].

The software in the system Matlab 5.1 was developed for implementation of such a procedure.

Calculation was made at the following initial data: the initial deviations of the furnace and metal ingot temperatures were, respectively. $\Delta T_{h0} = 30^{\circ}$ C, $\Delta T_0 = 60^{\circ}$ C, the holding temperature was 800° C, $A_1 = 6.11$ h⁻¹, $A_2 = 0.638^{\circ}$ C/m³, $A_3 = 3.45$ h⁻¹, $\mu = 0.69$ h⁻¹, $\alpha = \beta = \gamma = 1$, $t_f = 1$ h.

The deviation of the actual flow rate of fuel in an optimum heating process from the desired one at the prescribed holding temperature of the metal ingot and a graph of the optimum operating conditions of the furnace are depicted in Figs. 1 and 2, respectively.

NOTATION

 $T_{\rm h}(t)$, temperature of heating medium, ^oC; T(t), temperature of metal ingot, ^oC; ν , gas flow rate, m³/h; $t_{\rm f}$, finite holding time, h; A_1, A_2, A_3, μ , constants characterizing the dynamics of metal ingot heating; α, β, γ , weight coefficients larger than zero. Subscripts: f, finite; hom, homogeneous; inhom, inhomogeneous; T, transposing.

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